

# TYPE DRY FG

## Test report L.1207.P.920.COM

TEST REPORT FOR SPECIFIC THERMAL OUTPUT  
OF FLOOR HEATING CONSTRUCTION IN ACC. TO EN 1264  
LOAD DISTRIBUTION LAYER: 3 mm, PIPE: 10 x 1.3 mm



**IGE**  
Institut für  
GebäudenEnergetik



Universität Stuttgart

Lehrstuhl für  
Heiz-und  
Raumluftechnik



Stuttgart, 02.04.2009

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Acceptances from certification bodies: DINCERTOCO / RAL / AFNOR / BSI / AENOR





## SPECIFIC THERMAL OUTPUT TESTING IN ACC. TO EN 1264 PART. 2, FLOOR HEATING SYSTEM

### 1. TEST METHOD

The currently valid versions of the following documents form the basis for inspection and certification:  
 DIN EN 1264-2: Prüfverfahren (1/2009)  
 DIN EN 1264-4: Installation (11/2009)  
 DIN EN 1264-5: Berechnungsverfahren (1/2009)

### 2. INSTITUT:

Institut für GebäudeEnergetik Lehrstuhl für Heiz- und Raumlufttechnik der Universität Stuttgart  
 Pfaffenwaldring 35 - D-70569 Stuttgart-Vaihingen

### 3. CLIENT:

COMISA S.p.A. - Via Neziole, 27 - 25055 - Pisogne (Bs) - ITALY

### 4. MANUFACTURER:

Pipe: Jansen (Switzerland)  
 Panel: GF-Systemelement: der Auftraggeber

### 5. SYSTEM DESCRIPTION

trademark: SISTEMA DRY FG  
 construction: Type A  
 spacing in m: 0,100

#### Pipe:

material: JANOl en 10 x 1.2 mm PE-RT/EVOH/PE-RT  
 diameter: 0,010 m  
 thickness: 0,0013 m

#### Pipe embedded in the system plate (slot) and a thin layer of compensation

#### Test sample:

appr. 40 Inch x 40 Inch, plus master insulation boards with given resistance of  $R_{\lambda,B} = 0,14$  und  $R_{\lambda} = 0,09$  m<sup>2</sup>K/W

### 6. PROCEDURE OF TESTING

The temperature field of the floor surface is measured in order to determine the values  $\vartheta_{F,m}$  and  $\vartheta_{F,max}$ . The measurement is carried out when steady state conditions are reached and a temperature of both cooling plates of  $\vartheta_i = 20 \text{ °C} \pm 0,5 \text{ K}$  is maintained. Under these conditions the average temperature of the heating medium  $\vartheta_H$  is set to achieve a maximum floor surface temperature of  $\vartheta_{F,max} = 29 \text{ °C}$  (i.e.  $\vartheta_{F,max} - \vartheta_i = 9 \text{ K}$ ) and in this case the difference between the average temperature of the heating medium and the temperature of the cooling plates  $\vartheta_H - \vartheta_i = \Delta \vartheta_H = \Delta \vartheta_{H,N}$  (standard value) applies.

Given that  $(\vartheta_{F,max} - \vartheta_i) = 9 \text{ K}$  is maintained and the average temperature difference of the floor surface and the room is determined, this temperature difference is used within the basic characteristic curve and gives the standard specific thermal output. The standard specific thermal output  $q_{N}$ , together with the above determined corresponding value of the standard temperature difference  $\Delta \vartheta_{H,N}$ , gives the equation for the characteristic curve for  $R_{\lambda,B} = 0$ .

## 7. TEST RESULTS:

Standard specific thermal output calculated on basic characteristic curve in acc. to DIN EN 1264

measuring point	$^j F_{1,1}$	24,93	°C	$^j F_{1,10}$	23,88	°C	$^j F_{1,1}$	25,14	°C	$^j F_{1,10}$	24,64	°C
	$^j F_{1,2}$	26,28	°C	$^j F_{1,11}$	25,20	°C	$^j F_{1,2}$	26,64	°C	$^j F_{1,11}$	25,43	°C
	$^j F_{1,3}$	28,96	°C	$^j F_{1,12}$	29,04	°C	$^j F_{1,3}$	29,09	°C	$^j F_{1,12}$	28,88	°C
	$^j F_{1,4}$	25,19	°C	$^j F_{1,13}$	25,30	°C	$^j F_{1,4}$	26,86	°C	$^j F_{1,13}$	27,31	°C
	$^j F_{1,5}$	23,98	°C	$^j F_{1,14}$	23,79	°C	$^j F_{1,5}$	26,10	°C	$^j F_{1,14}$	25,58	°C
	$^j F_{1,6}$	24,91	°C	$^j F_{1,15}$	24,53	°C	$^j F_{1,6}$	27,04	°C	$^j F_{1,15}$	26,20	°C
	$^j F_{1,7}$	28,94	°C	$^j F_{1,16}$	28,85	°C	$^j F_{1,7}$	28,88	°C	$^j F_{1,16}$	29,11	°C
	$^j F_{1,8}$	24,67	°C	$^j F_{1,17}$	25,54	°C	$^j F_{1,8}$	25,82	°C	$^j F_{1,17}$	26,93	°C
	$^j F_{1,9}$	23,58	°C	$^j F_{1,18}$	24,62	°C	$^j F_{1,9}$	24,68	°C	$^j F_{1,18}$	25,37	°C
water inlet temperature	$^j C_{in}$	19,90	°C	$^j C_{in}$	19,91	°C						
	water outlet temperature	$^j C_{out}$	19,99	°C	$^j C_{out}$	20,06	°C					
	average surface temperature	$^j V$	34,30	°C	$^j V$	48,29	°C					
		max. floor surface temperature	$^j R$	34,14	°C	$^j R$	47,93	°C				
cooling plate temperature	$^j F_{m,1}$	25,85	°C	$^j F_{m,1}$	25,85	°C						
	excess temperature	$^j F_{max}$	28,95	°C	$^j F_{max}$	28,95	°C					
	excess temperature	$^j i$	19,95	°C	$^j i$	19,95	°C					
		$^j F_{max-q_i}$	9,00	°C	$^j F_{max-q_i}$	9,00	°C					
		$^j F_{m-q_i}$	5,90	°C	$^j F_{m-q_i}$	5,90	°C					
		$^j H$	14,28	°C	$^j H$	14,28	°C					

Experimental test results for EN 1264 - 2

$\vartheta_{H,N}$	$q_n$
14,28	62,9

Kennlinien des Systems $q = K_H \cdot \vartheta$					
$R_{\dots,B}$	0	0,05	0,10	0,15	$m^2K/W$
$K_H$	4,406	3,558	2,985	2,570	$W/m^2K$

Characteristic curves

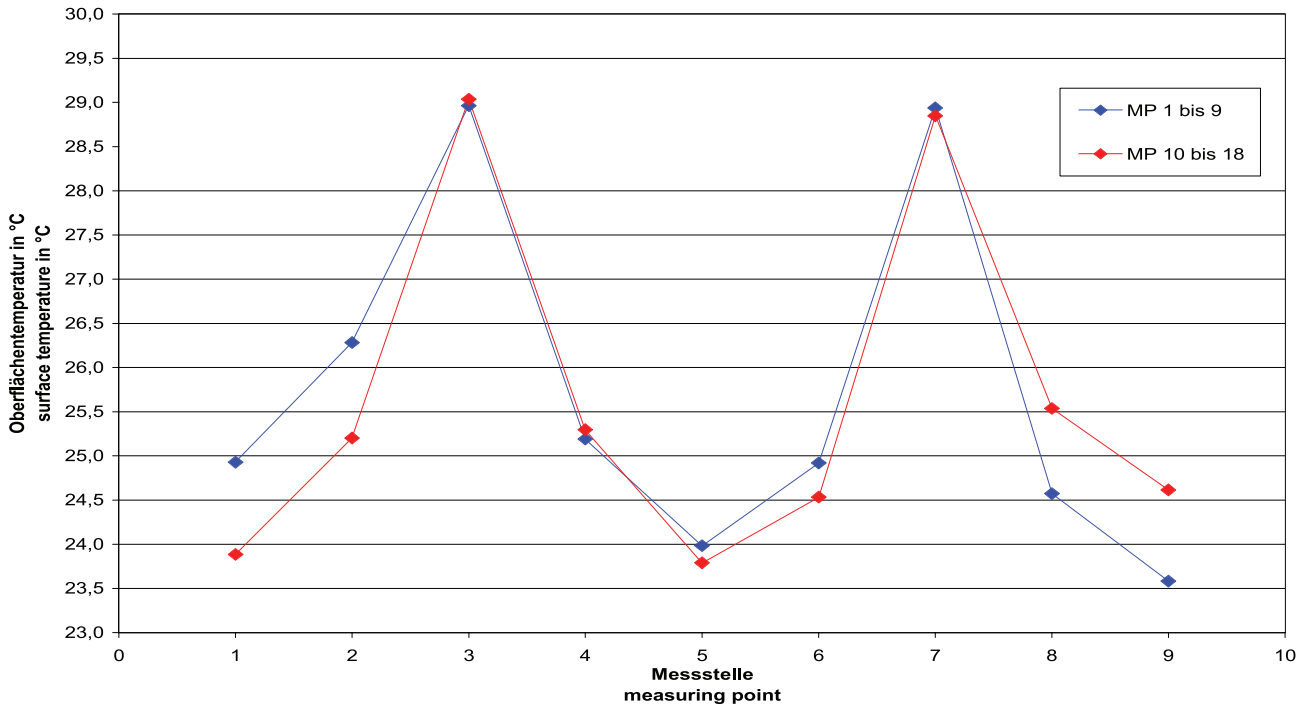
Grenzwärmestromdichte Aufenthaltsbereich: $(\vartheta_{F,max} - \vartheta_i) = 9K$					
$R_{\dots,B}$	0	0,05	0,10	0,15	$m^2K/W$
$q_G$	62,9	66,6	70,7	75,3	$W/m^2$
$\vartheta_{H,G}$	14,3	18,7	23,7	29,3	K

Limit specific thermal output in the **residence area**

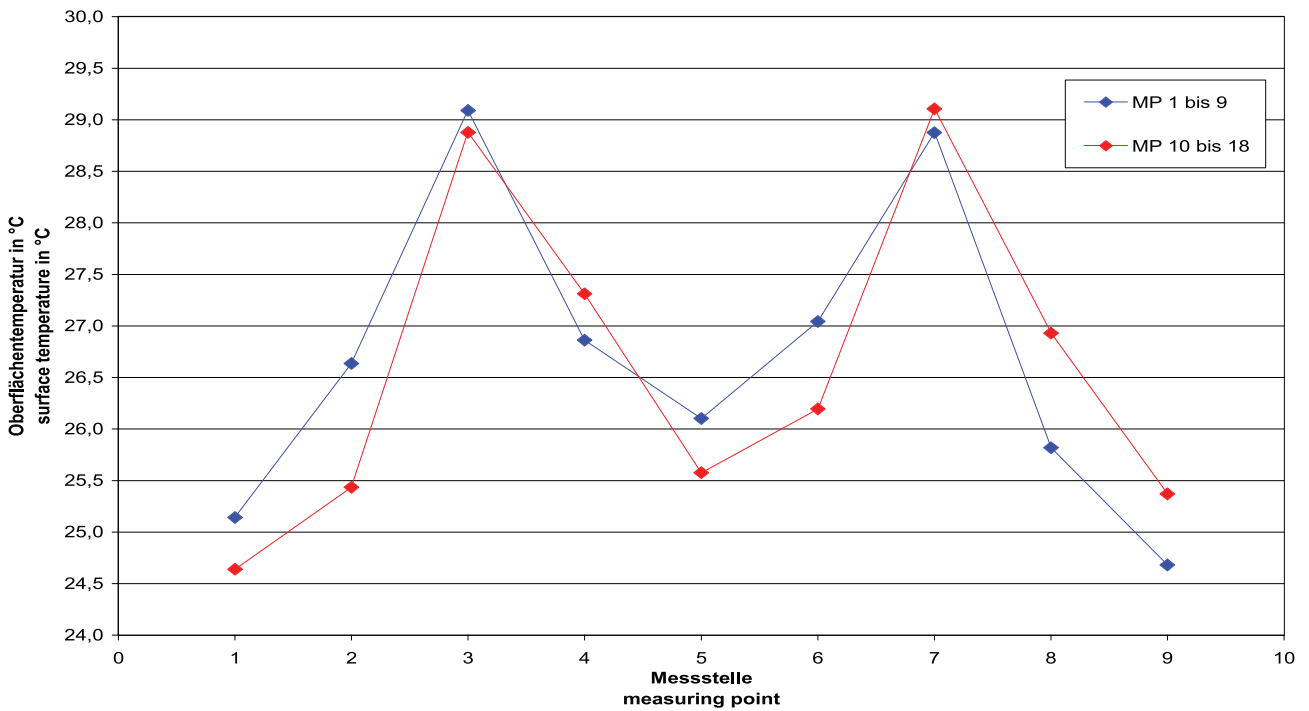
Grenzwärmestromdichte Randzone: $(\vartheta_{F,max} - \vartheta_i) = 15K$					
$R_{\dots,B}$	0	0,05	0,10	0,15	$m^2K/W$
$q_{G,R}$	110,3	116,7	124,0	132,1	$W/m^2$
$\vartheta_{H,G}$	25,0	32,8	41,5	51,4	K

Limit specific thermal output in the **peripheral area**

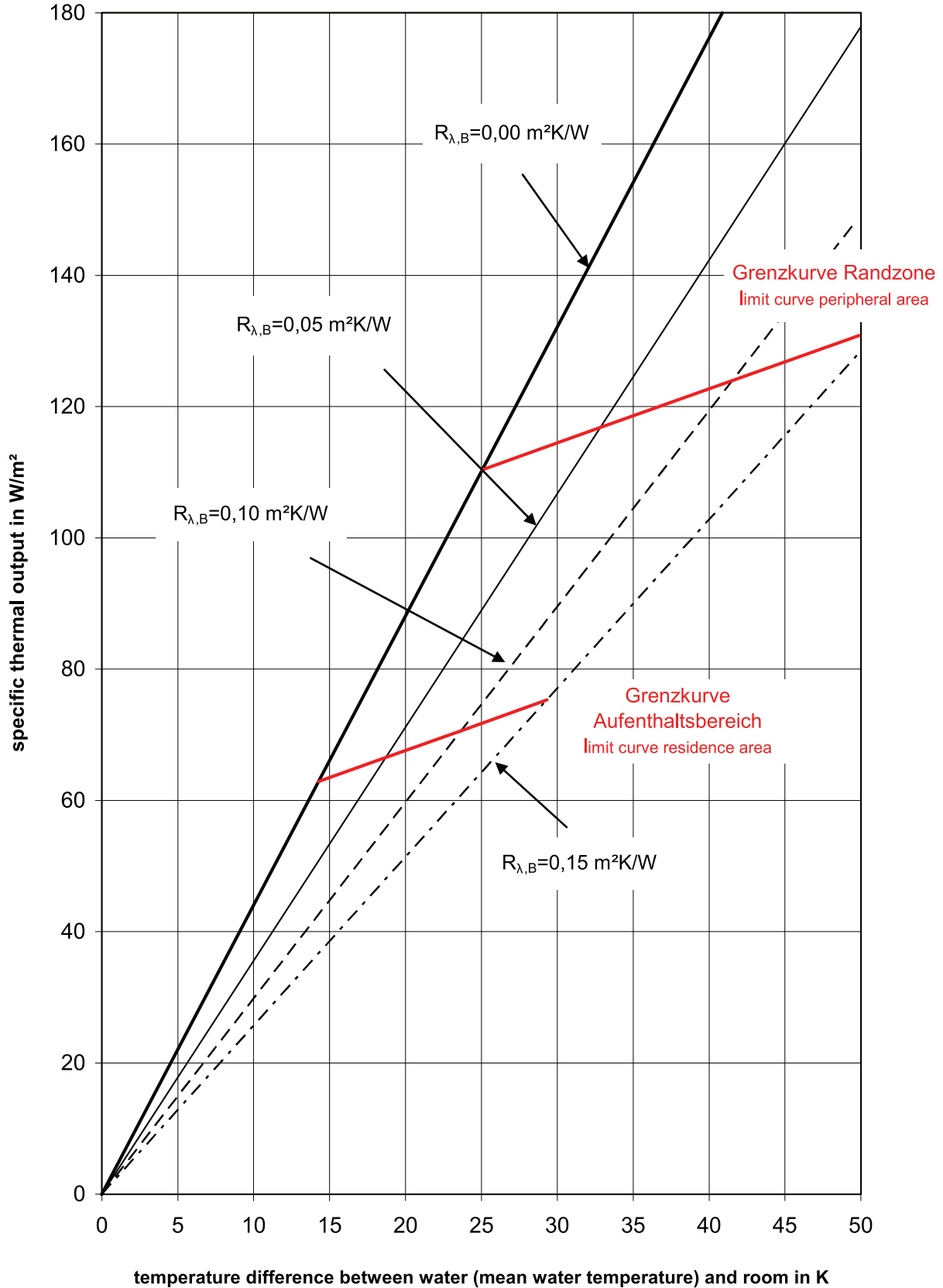
**Surface temperature without floor covering**



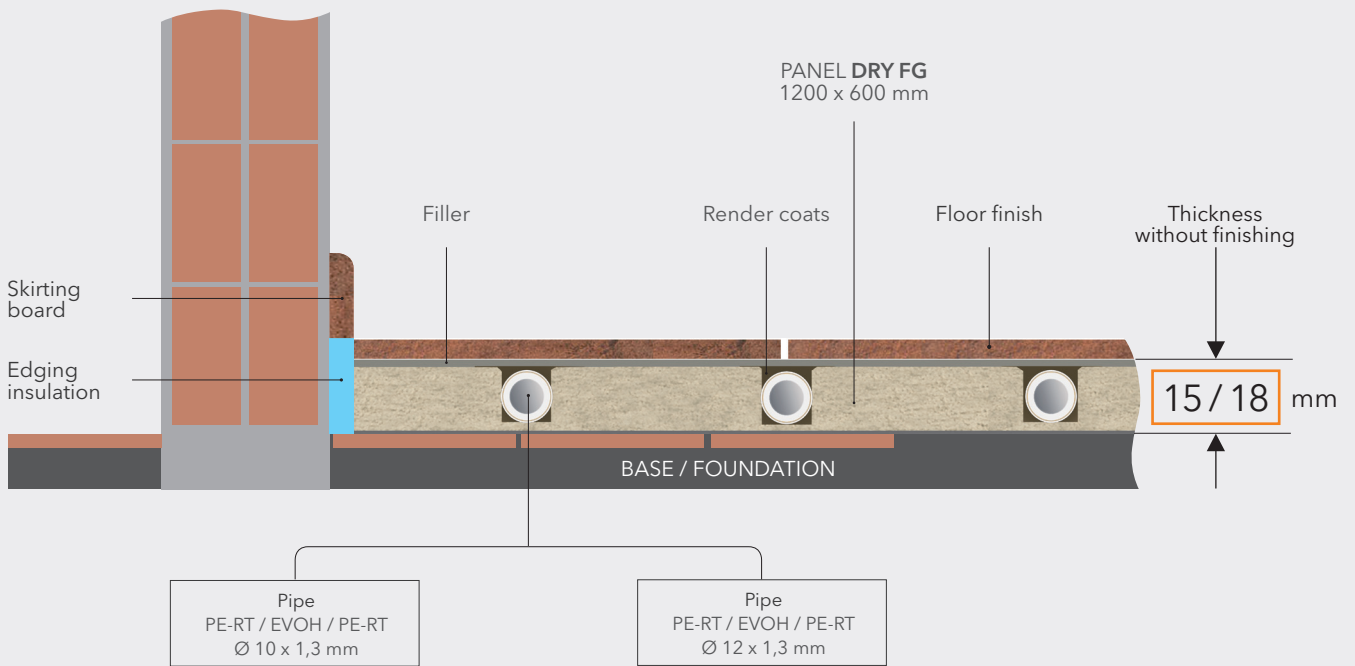
**Surface temperature with floor covering  $R\lambda, B = 0,14 \text{ m}^2\text{K/W}$**



Characteristic curves of the floor heating system

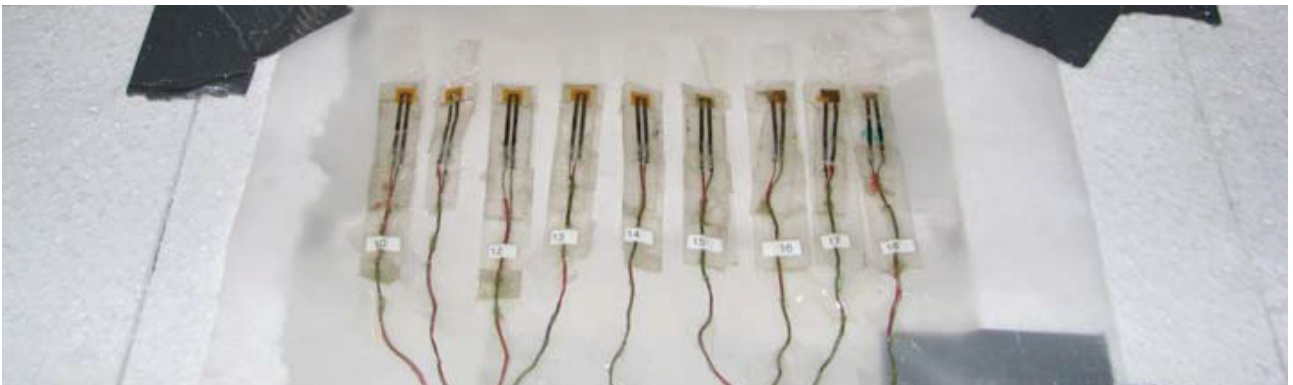


8. CONSTRUCTION DRAWING OF TEST SAMPLE:



## 9. PICTURE OF TEST AREA:

The test area was built in the Institut. The used material was sended directy by the client.  
The construction is equal to the nominal construction of the drawing and the technical documents.



## 10. CONFORMITY OF THE TECHNICAL DOCUMENTS

The system is type A of DIN 18560 part. 2.  
The sketch on the technical documents are in acc. to EN 1264 part. 4.  
The official technical documents should be sended to the Institut within 6 months.

# TYPE WET EPS

## Test report L.1207.P.923.COM

TEST REPORT FOR SPECIFIC THERMAL OUTPUT  
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LOAD DISTRIBUTION LAYER: 3 mm, PIPE: 10 x 1.3 mm



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Stuttgart, 30.04.2009

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**TEST METHOD:**

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DIN EN 1264-4: Installation (11/2009)  
DIN EN 1264-5: Berechnungsverfahren (1/2009)  
Zertifizierungsprogramm DIN CERTCO: (Raumflächen-integrierte Heiz- und Kühlsysteme mit Wasserdurchströmung“

**TEST ITEM:**

Type DRY FG, thin layer of compensation: appr. 3mm

**START - END OF TESTS:**

24.7.2012 - 24.07.2012

**MANUFACTURER:**

The Client

**TRADEMARK:**

DRY FG

**SYSTEM DESCRIPTION:**

Sondersystem mit Kunststoff-Rohren (siehe Abbildungen im Anhang dieses Berichtes)

**SYSTEM CONSTRUCTION:**

special system in acc. to DIN EN 1264

**DISTIBUTION LAYER:**

compensation layer: appr. 3mm

**PIPE:**

multilayer pipe 10 x 1.3mm PE-RT/EVOH/ PE-RT (producer: Saicompert, Switzerland)

**INSERTS:**

-

**PIPE FIXATION:**

Pipe embedded in the system place (slot)

**SPACING:**

100 mm

**TEST SAMPLE:**

appr. 40 Inch x 40 Inch, plus master insulation boards with given resistance of  $R_{\lambda,B} = 0,14$  und  $R_{\alpha} = 0,09$  m<sup>2</sup>K/W

**DATE OF RECEIPT:**

18.6.2012

## SPECIFIC THERMAL OUTPUT TESTING IN ACC. TO EN 1264 PART. 2, FLOOR HEATING SYSTEM

### 1. DECIPTION OF THE TEST METHOD:

The heating output of the looked floor system can be determined to EN 1264 part. 2. In part. 5 of EN 1264 instructions are given which changes are to be expected in the output (heating case and chilled case), if the arrangement of the space surfaces is changed. Thus the arrangement on the ground is, e.g., in the chilled case the case with the lowest output values, while in the heating case the arrangement on the ground proves the highest values.

### 2. TEST RESULTS:

#### 2.1 PROCEDURE OF TESTING:

The standard specific thermal output the heating case is calculated to EN 1264 for 4 standard layers ( $R_1$  to  $R_4$ ):

$$R_{\lambda} = 0,0; 0,05; 0,1 \text{ and } 0,15 \text{ m}^2 \text{ K/W}$$

These theoretical values of the resistance cover the really seeming floor covering to a great extent, so that for the later use with these values or interpolations the system can be laid out.

#### 2.2 RESULTS OF HEATING CASE IN ACC. TO EN 1264 PART. 2:

Characteristics of the system $q = K_h \cdot \Delta\theta$					
$R_{x,B}$	0	0,05	0,1	0,15	W/m <sup>2</sup> K
$K_H$	4,406	3,558	2,985	2,570	W/m <sup>2</sup> K

#### 2.3 RESULTS OF CHILLED CASE IN ACC. TO EN 1264 PART. 5:

The results for the floor heating system in acc. to EN 1264 part. 2 has to be transmitted by calculation method in acc. to EN 1264 part. 5

ADD. FLOOR COVERING	$\alpha$ (W/m <sup>2</sup> K)	$\Delta R_{\mu} = 1/\alpha - 1/10,8$ (m <sup>2</sup> K/W)
Spacing T	Equivalent coefficient for heat transfer $k_H$	
Floor	10,8	0,000 0
Floor	6,5	0,061 0
Wall	8,0	0,032 4
Wall	8,0	0,032 4
Ceiling	6,5	0,061 3
Ceiling	10,8	0,000 0

### 3 CHARACTERISTIC CURVES FOR THE CASE OF CHILLED FLOOR

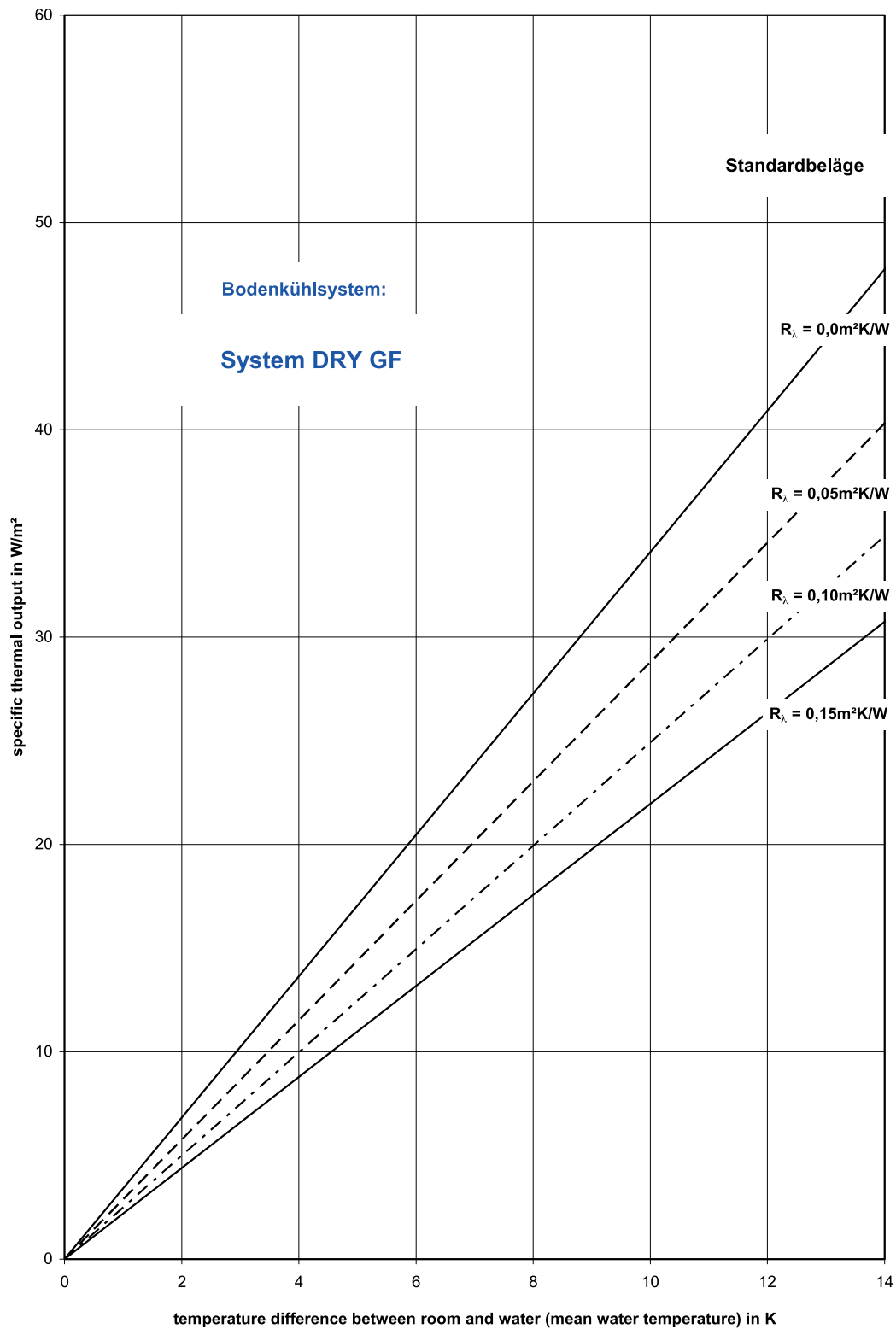
The cooling output of a floor system is reduced with the otherwise same conditions compared with the output of an under-floor heating system. A cause for this are the changed conditions on the heat transfer by convection on the surface of the floor. From part 5 on EN 1264 the respective heat transfer coefficients are known.

For the looked floor type WET EPS (covering: appr. 3mm, pipe: PE-RT, 10 x 1.3) the following output values arise.

$$q = k_H \cdot \Delta\theta_H \quad \text{with} \quad \Delta\theta \text{ Temperature difference}$$

Characteristics of the system $q = K_h \cdot \Delta\theta$					
$R_{x,B}$	0	0,05	0,1	0,15	m <sup>2</sup> K/W
$K_H$	3,410	2,880	2,492	2,196	W/m <sup>2</sup> K

Cooling output in dependence of the temperature distance room - water for pipe distance RA 100 mm



Prof. Dr.-Ing. M. Schmidt

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